

In the Specification

Please amend the paragraph at page 1, lines 12 - 17, as follows:

- - Various problems as described above arise when a rotary polygon mirror is used to scan a light beam. Moreover, there is a limitation as to both the scanning speed and acceleration of a rotary polygon mirror. Imaging techniques that are equivalent in result to scanning a laser light without using a rotary mirror have been investigated to further enhance the image-forming speed. When such techniques are used, beams from laser light sources need to be accurately guided onto a surface, and thus the development of ~~an laser~~ a laser array imaging lens suited to this task is required. - -

Please amend the paragraph at page 1, lines 18 - 21, as follows:

- - Image-forming devices that use a so-called semiconductor laser array made by arraying multiple light emitting elements in rows as a light source and that use a laser array imaging lens that images light beams from such a light source onto a surface to be scanned are described in Japanese Laid-Open Patent Applications H10-16297 and 2000-249915. - -

Please amend the paragraph at page 15, lines 28 - 35, as follows:

- - Figs. 6A - 6D show the spherical aberration, astigmatism, distortion and lateral color, respectively, for this embodiment. The spherical aberration (in mm) is shown for the wavelengths 770 nm, 780 nm and 790 nm, the astigmatism (in mm) is shown for both the sagittal S and tangential T image surface, and the lateral color (in mm) is shown for the wavelengths 770 nm and 790 nm. The f-number  $F_{No}$  of this embodiment is listed in Fig. 6A and the maximum ray height  $y' = 105$  mm is listed in Figs. 6B - 6D. Fig. 6E shows the coma (in mm) for ray heights  $y'$  of zero, 73.5 mm and 105 mm. As is evident from Figs. 6A - 6E, all these aberrations are favorably corrected for a wavelength of 780 nm. As is evident from Fig. 6C, distortion does not exceed 2%.

Please amend the paragraph that spans pages 17 - 18, as follows:

- - Figs. 7A - 7D show the spherical aberration, astigmatism, distortion and lateral color, respectively, for this embodiment. The spherical aberration (in mm) is shown for the wavelengths 770 nm, 780 nm and 790 nm, the astigmatism (in mm) is shown for both the sagittal S and tangential T image surface, and the lateral color (in mm) is shown for the wavelengths 770 nm and 790 nm. The  $F_{NO}$  of this embodiment is listed in Fig. 7A and the maximum ray height ( $y' = 105$  mm) is listed in Figs. 7B - 7D. Fig. 7E shows the coma (in mm) for ray heights  $y'$  of zero, 73.5 mm and 105 mm. As is evident from Figs. 7A - 7E, all these aberrations are favorably corrected, with the spherical aberration and lateral color aberration being much improved for the wavelengths 770 nm and 790 nm by the action of the DOE surface having a phase function being superimposed on a rotationally symmetric, aspheric surface. As is evident from Fig. 7C, distortion does not exceed 2 %. This embodiment enables the maintaining of satisfactory imaging properties even if a fluctuation of wavelengths occurs among one or more of the semiconductor laser array elements. - -